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					HC/	HCS -	- Spir	dles			
	Spino	lle	type	Housing diameter [mm]	Max. speed [rpm]	Output [kW]	From speed [rpm]	Torque [Nm]	Lubrication	Tool interface	Bearing W1 [mm]
HC	80 cg	-	40000/3	80	40000	3	30000	0.96	g	HSK - E 25	30
HC	100 cg	-	30000/3	100	30000	3	14400	2	g	HSK - E 32	40
HCS	120	-	45000 / 15	120	45000	15	24000	6	OL	HSK - E 40	45
HCS	120	-	60000 / 12	120	60000	12	51000	2.3	OL	HSK - E 25	30
HCS	120	-	75000 / 10	120	75000	10	75000	1.3	OL	HSK - E 25	30
HCS	150	-	42000 / 30	150	42000	30	21000	13.7	OL	HSK - E 50	55
HCS	150	-	42000 / 32	150	42000	32	30000	10.2	OL	HSK - E 50	55
HCS	170	-	24000 / 41	170	24000	41	7000	56	OL	HSK - A 63	70
HCS	170	-	28000 / 40	170	28000	40	7000	54.5	OL	HSK - A 63	70
HCS	170	-	40000/39	170	40000	39	18000	20.7	OL	HSK - E 50	55
HCS	180	-	24000 / 27	180	24000	27	18000	14.5	OL	HSK - A 63	70
HCS	200	-	30000 / 15	200	30000	15	12000	12	OL	HSK - A 50 / E 50	55
HCS	200	-	30000 / 46	200	30000	46	15000	29.3	OL	HSK - E 63	70
HCS	230	-	12000 / 30	230	12000	30	1600	179.3	OL	HSK - A 100	110
HCS	230	-	22000 / 120	230	22000	120	13800	83.5	OL	HSK - A 80	90
HCS	230	-	24000 / 18	230	24000	18	3150	57	OL	HSK - A 63	70
HCS	230	-	30000/80	230	30000	80	16500	46.5	OL	HSK - A 63	70
HCS	230	-	40000 / 22	230	40000	22	10000	21	OL	HSK - E 50	55
HCS	230 g	-	10000 / 24	230	10000	24	2500	91.7	g	HSK - A 63	90
HCS	230 g	-	16000 / 24	230	16000	24	6000	38.2	g	HSK - A 63	70
HCS	270	-	15000 / 80	270	15000	80	5340	143.5	OL	HSK - A 100	110
HCS	285	-	12000 / 32	285	12000	32	1000	306	OL	HSK - A 100	110
HCS	285	-	12000 / 40	285	12000	40	1680	227.5	OL	HSK - A 100	110
HCS	300	-	12000 / 30	300	12000	30	1000	270	OL	HSK - A 100	110
HCS	310	-	12000 / 25	310	12000	25	930	256.7	OL	HSK - A 100	110
HCS	320	-	8000 / 40	320	8000	40	1050	380	OL	SK 50	110

Max. power \$1 [kW]Max. speed [rpm]

Housing diameter [mm] Spindle type

HC = for open-loop drive HCS = for closed-loop drive W1 = Bore diameter of front bearings

OL = Oil/air lubrication

g = Permanent grease lubricatiion

SK = ISO taper

HSK = Hollow tapered shank

Preference type

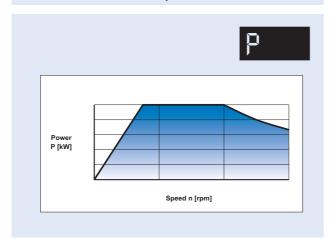
Spindles for oil/air lubrication are also available as spindles with permanent grease lubrication. Please ask for speed reduction in these cases.

Please ask if spindle drawing is required. We send it as dxf file.

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Shaft Output Power



Chip removal rates are defined by the material's specific cutting speeds. Generally small tool diameters require high speeds and larger tools are operated at lower speeds.

Large tools require high torque while small tools require less torque, but higer speeds.

Integral motors utilized in the HC/HCS style spindle meet these requirements.

The "field weakening" characteristics provide the high torque at lower speed.

The spindles can be operated in the following modes:

- ➤ S1 Continuous power
- ➤ S6 Continuous duty with intermittent loading, a duty factor of 60% (S6-60%) for a cycle time of 2 minutes.

Depending on the application requirements, the motor characteristics curve of power / torque relative to speed can be met.

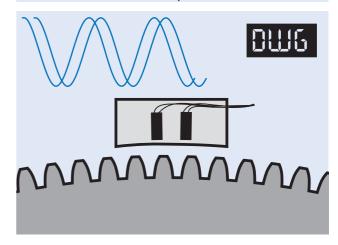
Rigidity is a prerequisite for the volume of metal to be removed and the surface finish required. This requires large shaft diameters, and accordingly large spindles, thereby large motors can be utilized.

Due to the advances in motor development, the power density has been increased to such an extent that in many cases the output power far exceeds the application requirements.

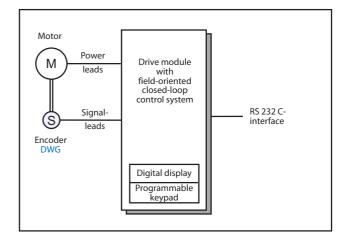
Oversized systems are costly, due to the size of the frequency inverter's required to operate them.

Therefore operating the spindles at the required power level, the capacity of the inverter determines the power profile.

Integral Encoders For Closed Loop Control



Incorporating high resolution encoders into spindles, provides feedback and control of the actual shaft speed, and angular position of the shaft, at all times.



The advantages are as follows:

- Smooth precise rotation and control at low speed
- ▶ "C"-axis operation e.g. thread cutting
- ▶ Shaft positioning within 0.001 degree
- ➤ The drives high dynamic performance at full capacity, combined with the quick acceleration and deceleration times, allows the systems full power capacity to be utilized.

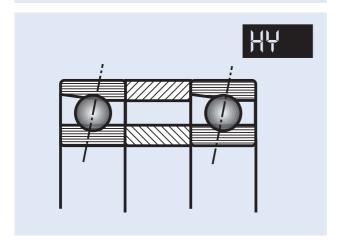
GMN can interface the encoders to meet the selected drive systems requirements.

The encoder system consists of a precision gear mounted to the rotating spindle shaft and a stationary sensor in the spindle housing readily accessible, for ease of service.

GMN will optimize the performance of the complete spindle and drive package before shipment, and provide all the necessary parameters.



Advantages Of Hybrid Ceramic Bearings



GMN "HC/HCS" series high frequency spindles utilize hybrid ceramic ball bearings. These bearings have standard steel bearing races and are matched with silicon nitride balls.

Advantages of Hybrid bearings compared with normal spindle bearings are:

Reduced wear

The high degree of hardness of the balls, and the nongalling effect of the silicon nitride against metallic material lessens the wear. This is especially important in cases of minimal lubrication. In addition, wear particles will not embed themselves into the balls to further damage of the races.

Riaidity

Modulus of elasticity is bigger than steel, which increases the static and dynamic stiffness. The increase in dynamic rigidity depends on the ratio of bearing preload to the centrifugal force on the balls.

Friction

Because of the reduced spin-rolls ratios and lower Hertzian stresses, friction and respectively operating temperatures are reduced.

Axial shaft movement

As a result of the lightweight ceramic balls, centrifugal forces are reduced with a corresponding reduction in dynamic movement of bearing races. In addition, movements due to less friction and the lower coefficient of expansion of ceramics are reduced.

Reliability of operation

The low thermal coefficient of expansion of the ceramic balls lessens the reduction of the radial running fits in the bearings. These fits are less variable at higher temperature differences between races.

Vibrations

Radial forces and the moments acting on the bearings produce displacement between the balls and the retainer. Hybrid bearings reduce this effect and produce a positive influence on cage vibrations and stresses.

Fatique life

The fatique life is comparable when the Hertzian stress on the contact surfaces between rings and balls is similar. As a result of the minor weight of the ceramic balls the Hertzian stress is lower.

Therefore hybrid bearings achieve longer life time.

Accuracy

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Spindles of HC family are fitted with bearings produced according to GMN standard grade UP. They are distinguished from international standards due to excellent running accuracy.

Radial runout of assembled bearing inner ring Limits in micron

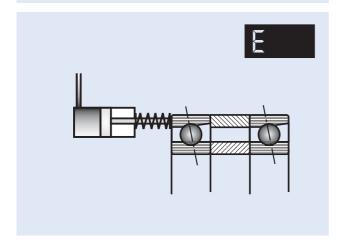
Bearing bore diameter [mm]	Toler P4/ABEC 7	UP	
> 2.510	2.5	1.5	1.5
> 1018	2.5	1.5	1.5
> 1830	3.0	2.5	1.5
> 3050	4.0	2.5	2.0
> 5080	4.0	2.5	2.0

Assembled bearing outer ring face runout with raceway axial runout - Limits in micron

Bearing outside diameter [mm]	Tolerance class P4/ABEC 7 P2/ABEC 9 UP		
> 6 8	5.0	1.5	2.0
> 18 30	5.0	2.5	2.0
> 30 50	5.0	2.5	2.0
> 50 80	5.0	4.0	3.0
> 80120	6.0	5.0	3.0



Adjustable Bearing Preload



Bearing arrangement and preload determine the rigidity, and influence the life time of the spindle system.

For small speed ranges, and low speed operation the different versions of a solid preload arrangement are suitable.

Large speed range variances, and high speed spindles, require a systems that will not allow the bearing preload to be influenced by either temperature or speed. These applications require spring preloading of the bearings.

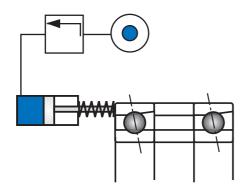
The above mentioned arrangements <u>cannot</u> be adjusted or changed, without disassembling the spindle.

With the "Adjustable bearing preload" system the bearing preload can be optimized to the application, and prolong the lifetime of the spindle.

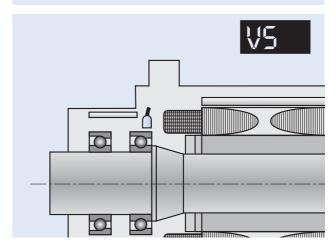
The base preload of the bearings is determined by the highest speed requirements, and is set by spring preloading.

preloading.
The optimized settings over the speed range is varied through an internal piston which is actuated via either hydraulic or pneumatic pressure.

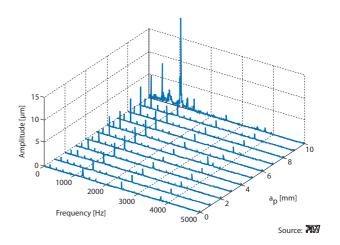
As further advantage of the adjustable preload system is reduction of vibration.



Vibration Sensor



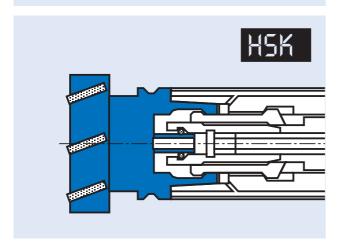
Unmonitored vibration can cause major damage to the spindle, machine tool and component being machined. GMN can provide sensors close to the front bearing set, which will quickly recognize any unbalance or high resonance which can cause catastrophic damage and shut-down the machine, or can plot out the curve on a display unit for analyzation and correction of the process or problem.



The illustration shows a spike in the vibration spectrum at 1000 Hertz at a 10 mm depth of cut. This vibration could be from extreme cutting loads, unbalanced tooling, or damaged spindle bearings.



Tool Interface



GMN can provide high frequency spindles to accept common tooling interface configurations.

The prefered HSK style offers the following advantages versus the ISO taper:

- ► High static and dynamic rigidity
- ▶ High tool change accuracy and repeatability
- ▶ Low axial movement during speed variations
- ▶ Increased pull-in force as the speed increases
- ► High torque transmission
- ► Increase in personal safety due to the internal drive dogs (Form A/C)

"Hollow tapered shanks with flat contact surfaces" are standard per DIN 69893. The different "FORMS" of a particular size are based on a similar shank size dimension. The tool flange is dictated by the mode of tool change.

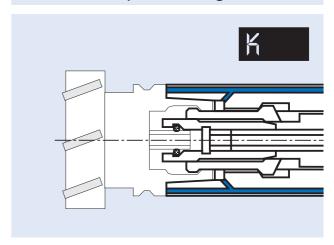
HC/HCS style spindles allow the use of tools with hollow shanks, type A, E or F according to interface design.

Form E was developed for high speed without drive dogs. The torque transmission is actuated by adherence.

Form A can also be used with manual tool change system provided in the HSP style spindles. This reduces the need for additional tool holders.

Tools according to Form B/D cannot be used in the HC/HCS spindle, they are designed for different applications.

Taper Cleaning



The high demand to precision requires excellent cleaness at the tool interface. Automatic tool changing system call also for automatic cleaning systems.

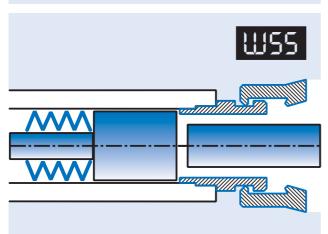
ISO taper cleaning can be operated at the taper surfaces whereas the HSK request also treatment of the plane face when the size it accepts.

In accordance to the interface size different systems can be used:

- ▶ Only air
- ▶ Air or coolant in one line
- Air and coolant in seperate lines



Clamping System



Both the ISO taper style and the "HSK" hollow shank tool holders are clamped via a set of gripper fingers. The clamping forces are generated through a spring washer pack, included in the power drawbar.

The centrifugal forces exerted by the balls in the pressure intensifier, multiplies the pull in force on an ISO taper style system. It is also speed dependent.

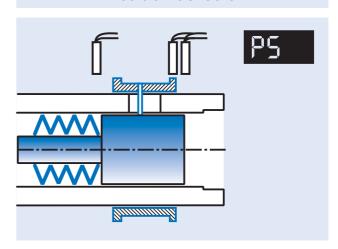
Increases in the pull in force for the HSK style tool clamping system is by the centrifugal forces on the internal gripping mechanism.

Tool un-clamping on either system is accomplished by actuating an internal piston with either hydraulic or pneumatic pressure.

An internal cylinder mounted at the rear of a spindle, along with a gripping mechanism supports the shaft during unclamping, to prevent the pressure exerted through the shaft from damaging the spindle bearings. During operation the gripping mechanism is disconnected.

These designs provide low vibration and a high safety factor for high speed quick change tool clamping systems.

Position Sensors



The GMN spindles are equipped with proximity sensors to allow for proper, trouble free operation during tool changing.

▶ Tool change

Depending on the size and nominal speed of the spindle, a variety of sensor arrangements can be applied for feed back to the machine control, about the tool changing cycle.

Variation A

A (2) two sensor arrangement for monitor the position of the piston, either "forward" or "back".

Variation B

Depending on the internal space constraints the drawbar can be monitored for "tool clamped", "unclamped", "clamped no tool", with (3) inductive proximity switches or one analog sensor.

Variation C

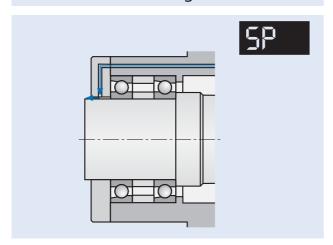
By utilizing the "taper cleaning" feature the air flow can also provide a signal that tool is improperly sized or not clamped correctly. This method can increase tool changing times.

► Rotation of shaft

If the spindle size and speed restrict the use of an encoder, GMN can provide alternative sensors for actual shaft speed, and also "zero speed".



Air Purge



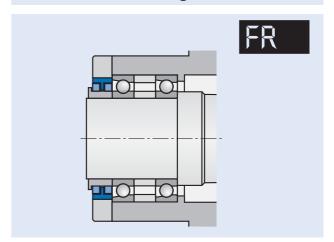
Pressurized air is used to prevent the ingress of

contamination into the bearing system.

A continuous flow of clean dry air fills the closely machined gaps between the stationary and rotating members of the spindle.

The air stream also stops the spent oil lubrication from existing at the front of the spindle and away from the work piece.

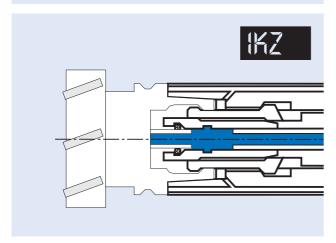
Fluid-Ring Seal



GMN has patented a "Fluid Ring" seal which can be incorporated in most GMN spindle designs, can operate in heavy external coolant and dust conditions, is **NO** speed limitations, and requires NO air.



Coolant Through Shaft

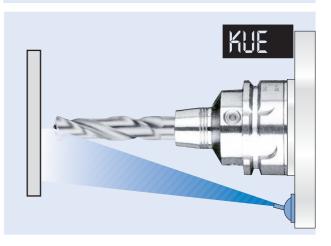


The internal coolant supply provides cooling directly to the cutting edge also at difficult form of workpieces.

In accordance to the interface size and dependent on the maximum operating speed different systems can be used:

- ▶ Only air
- ▶ Air or coolant in one line
- ► Air and coolant in seperate lines

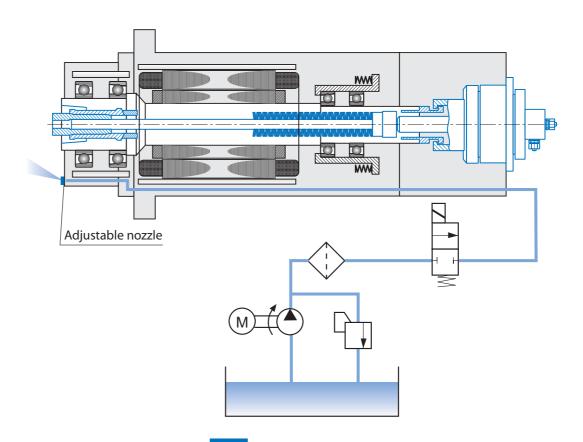
Coolant Through Spindle Housing



For cooling of tool and workpiece the medium is supplied through spindle housings and nozzels to the cutting surfaces.

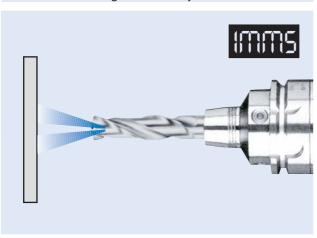
Compressed air, cooling lubricant/air mixture or cooling lubricant can be used.

The representation below is with cooling lubricant as medium.



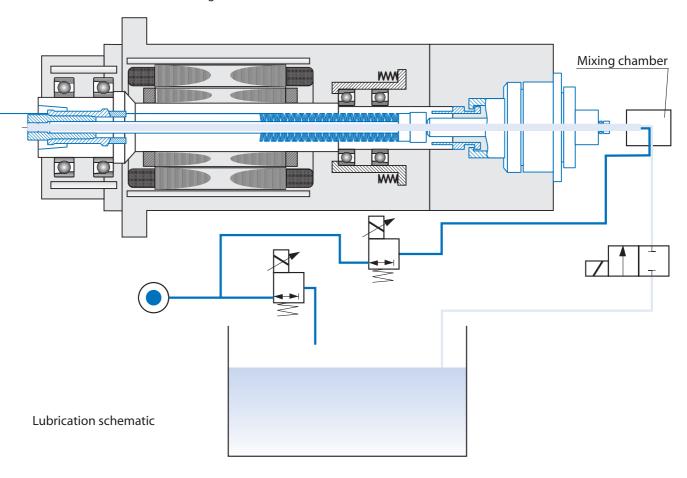


Internal Minimized Coolant Supply Single-Channel System



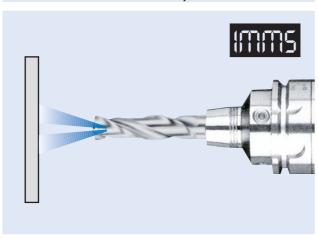
Characteristics of single-channel minimized coolant supply:

- ► Superfine oil mist (aerosol)
- ▶ Speed limitation due to aerosol decomposition
- For standard rotary unions
- ► For tools with coolant bore diameter > 1 mm
- ► In comparison with two-channel system longer reaction times at quantity changings
- ► For machines with less tool changes



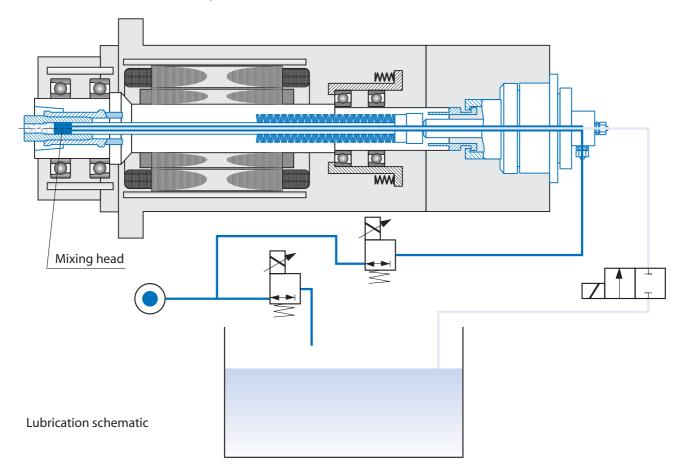


Internal Minimized Coolant Supply Two-Channel System



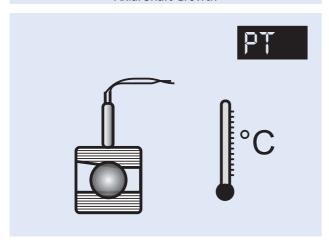
Characteristics of two-channel minimized coolant supply:

- ▶ No oil mist
- Oil and air mixable in almost any quantities or only air supply
- ▶ In comparison with single-channel system higher speeds possible
- ▶ For tools with high lubricant consumption
- ► For machines with more tool changes



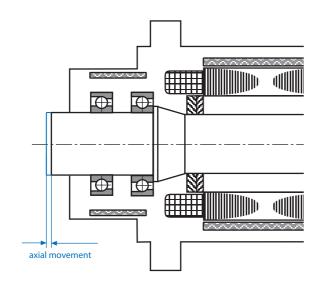


A Method For Controlling Axial Shaft Growth



Precision machining requires the position of the cutting edge of the tool to be maintained.

Temperature variations and centrifugal forces at the balls and bearing races, can cause axial movement of the tool mounting face of the shaft.

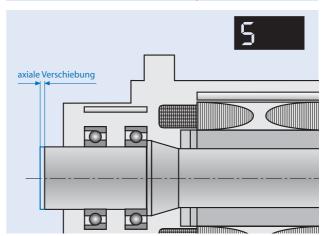


The "centrifugal forces" factor can be calculated and the speed dependent shaft movement can be compensated by through the machine tool control.

Measuring the shaft temperature at the bearing during operation is difficult.

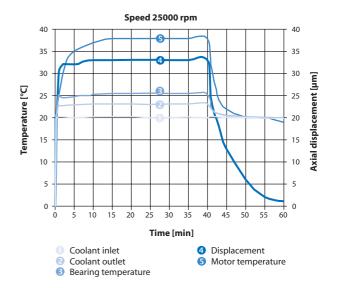
Experience has shown that by measuring the temperature at outer diameter of the bearings, approximate temperature variations can be established and the axial movement compensated for.

Measurement Of The Axial Shaft Growth By Sensor



Axial shaft growth which is caused by fluctuations in temperature, can produce process errors in milling applications. GMN can incorporate a sensor at the front of the spindle to record the exact growth and the CNC machine control can compensate for the movement.

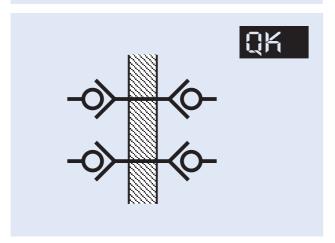
The measuring system which consists of an electronic controller which conditions the signal provided by the sensor has data storage capacity which provides immediate response after spindle exchange.



The diagram illustrates the axial shaft growth of a spindle operating at 25000 rpm.



Pick-up Spindle ★ Multi Couplings

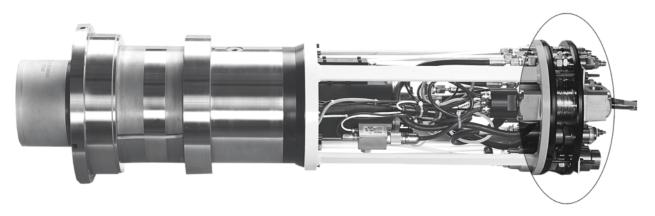


GMN spindles can be supplied with multi-couplings for energy and fuel supply.

This reduces the unproductive spindle replacement times, or - depending on the design - can even make possible the automatic replacement of spindles, thus increasing the flexibility of the machine.



Quick Couplings





Spindle Testing Stand



Before GMN machine spindles for high speed machining (HSC) are delivered, they are tested on a test stand specially developed for GMN.

One reason for this is that motor spindles become more and more complex and on the other hand their reliability is guaranteed by this.

The test in which the setpoints as well as cycle and switching times are specified runs automatically. Finally a test certificate is produced in which all measured values are documented.

2 motor spindles with different parameters can be tested simultaneously.

Here it was proven that 180 cycles are sufficient to guarantee the highest possible reliability. In every cycle the spindle is turned to maximum speed in a specified time within seconds, the shaft encoder signals are checked, the spindle is braked under defined conditions after a certain time, the tool change is performed and the signals of the position sensors are

The position of the tool clamping system can be determined optionally analogously or through individual switches

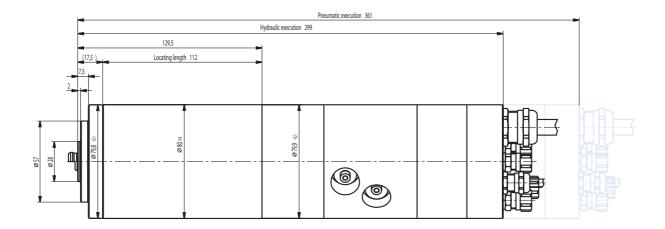
Furthermore the following are acquired: motor current, voltage in the windings, temperature of the winding and of the foremost bearing and, depending upon spindle equipment, functioning of coolant supply through the shaft and the adjustable bearing preload.

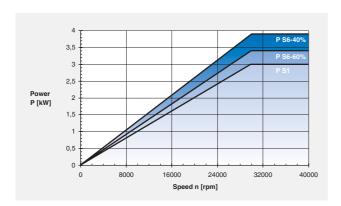
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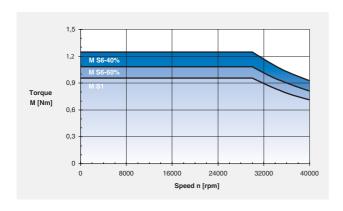
16



HC 80cg - 40000/3







Synchronous motor

Power P (S1)	3 kW at 30,000 rpm
Torque M (S1)	0.96 Nm
Speed n _{max}	40,000 rpm
Drive	

Hybrid ball bearings

bore diameter	
of front bearings	30 mm
Lubrication	Grease

Tool interface

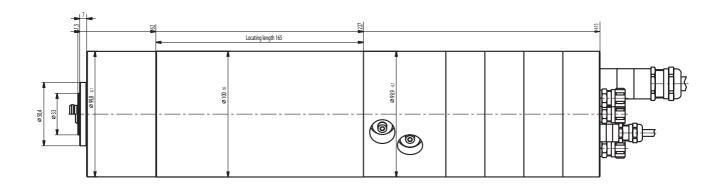
Interface Monitoring	HSK-E 25
"clamped", "unclamped"	Analog sensor
Taper cleaning	
Static tool pull-in force	
Tool release	Hydraulic or
	pneumatic
Seal	Air purge

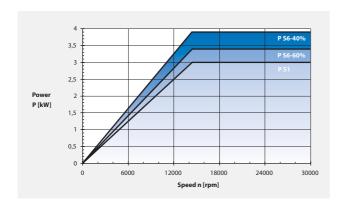
Rigidity

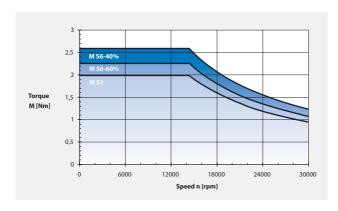
Radial	89 N/μm
Axial	120 N/μm



HC 100cg - 30000/3







Synchronous motor

Power P (S1)	3 kW at 14,400 rpm
Torque M (S1)	2 Nm
Speed n _{max}	30,000 rpm
Drive	open-loop

High precision hybrid ball bearings

Bore diameter	
of front bearings	40 mm
Lubrication	Grease

Tool interface

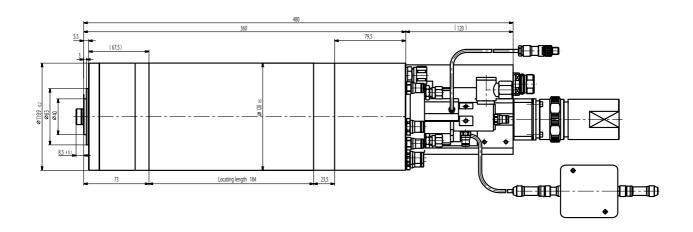
Interface	HSK-E 32
Monitoring	
"clamped", "unclamped" .	Proximity switches
Seal	Air purge

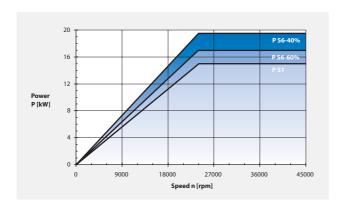
Rigidity Radial

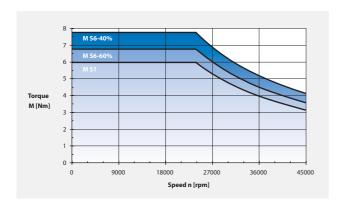
ugiaity	
Radial	105 N/μm
Axial	50 N/µm



HCS 120 - 45000/15







Synchronous motor

Power P (S1)	15 kW at 24,000 rpm
Torque M (S1)	•
Speed n _{max}	45,000 rpm
Drivo	closed-loop

Hybrid ball bearings

,	
Bore diameter	
of front bearings	45 mm
Lubrication	

Tool interface

Coolant	
Seal	Air purge
Static tool pull-in force	6.8 kN
Taper cleaning	Air
"clamped without tool"	Proximity switches
"clamped", "unclamped",	
Monitoring	
Interface	HSK-E 40

Coolant

through shaft80 bar

Shaft movement

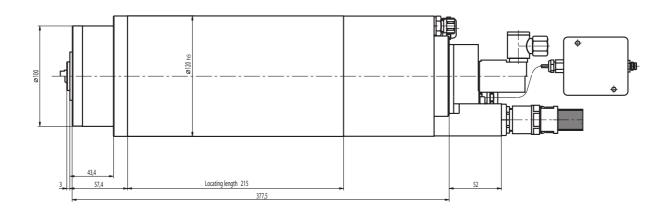
Compensating - AxialTemperature sensor

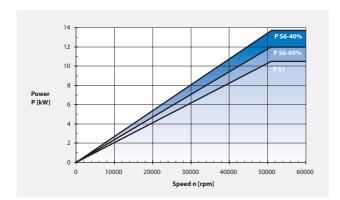
Rigidity

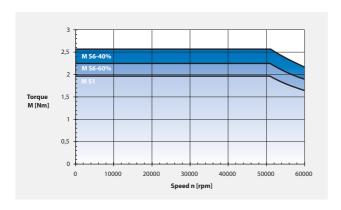
Radial 125 N/μm Axial91 N/μm



HCS 120 - 60000/12







Asynchronous motor

Power P (S1)	12 kW at 51,000 rpm
Torque M (S1)	2.3 Nm
Speed n _{max}	
Drive	

Hybrid ball bearings

Bore diameter	
of front bearings	.30 mm
Lubrication	.Oil/air

Tool interface

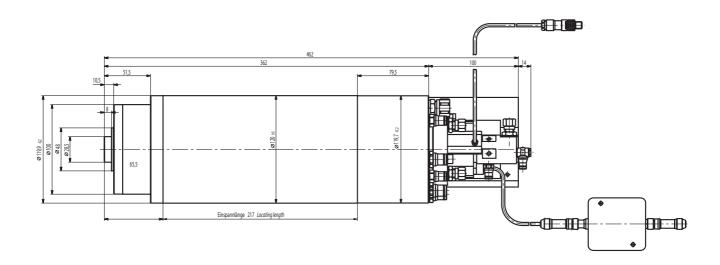
Interface	HSK-E 25
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	2.8 kN
Seal	Air purge
Coolant	
through shaft	80 bar

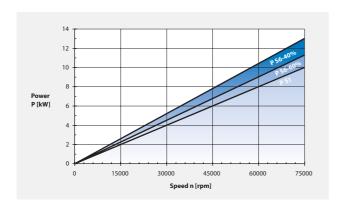
Rigidity

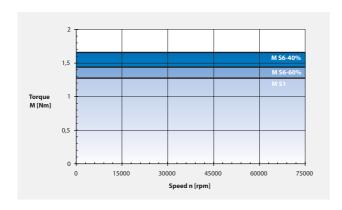
Radial	110 N/µm
Axial	70 N/µm



HCS 120 - 75000/10







Synchronous motor

Power P (S1)	10 kW at 75,000 rpm
Torque M (S1)	1.3 Nm
Speed n _{max}	75,000 rpm
Drive	closed-loop

Hybrid ball bearings

•	_	
Bore diameter		
of front bearings	s	30 mm
Lubrication		

Tool interface

Interface	HSK-E 25
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	2.8 kN
Seal	Air purge

Coolant

through shaft80 bar

Shaft movement

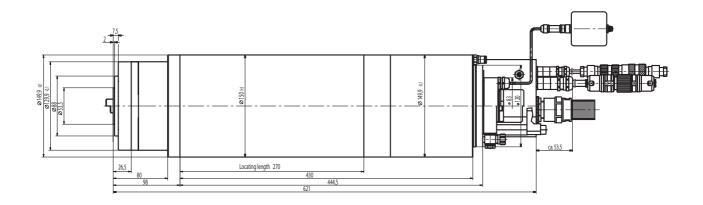
Compensating - AxialTemperature sensor

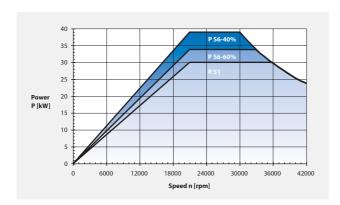
Rigidity

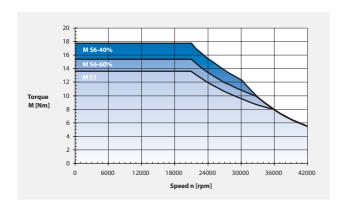
Radial110 N/μm Axial69 N/μm



HCS 150 - 42000/30







Synchronous motor

Power P (S1)	30 kW at 21,000 rpm
Torque M (S1)	
Speed n _{max}	42,000 rpm
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	55 mm
Lubrication	Oil/air
Bearing preload	adjustable

Tool interface

Interface	HSK-E 50
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	7.5 kN
Seal	Air purge

Shaft movement

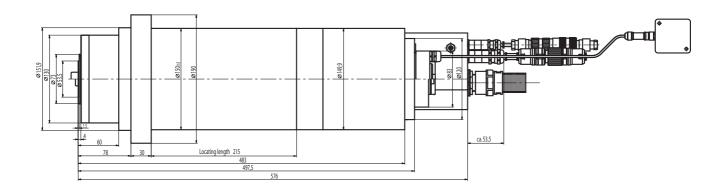
Compensating - Axial	Temperature sensor
Measuring - Axial	Displacement sensor
Measuring - Radial	2 Displacement
	sensors

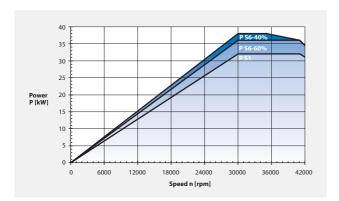
Rigidity

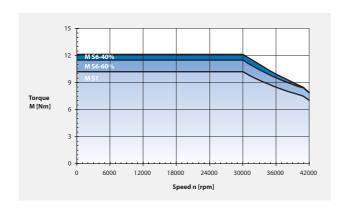
Radial	162	N/µm
Axial	128	N/um



HCS 150 - 42000/32







Asynchronous motor

Power P (S1)	32 kW at 30,000 rpm
Torque M (S1)	10.2 Nm
Speed n _{max}	
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	55 mm
Lubrication	Oil/air

Tool interface

Interface	HSK-E 50
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	7.5 kN
Seal	Air purge

Shaft movement

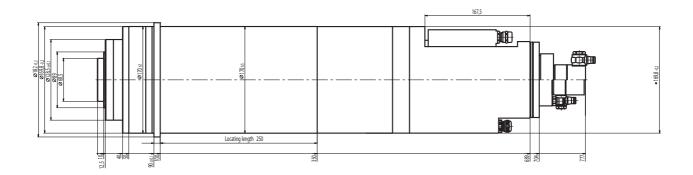
Compensating - Axial .	Temperature sensor
Measuring - Axial	Displacement sensor

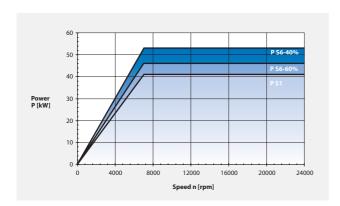
Rigidity

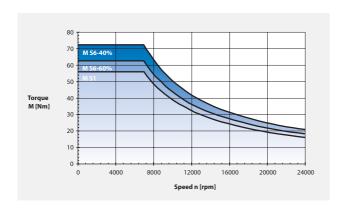
Radial	225	N/µm
Δvial	128	N/um



HCS 170 - 24000/41







Synchronous motor

Power P (S1)	41 kW at 7,000 rpm
Torque M (S1)	56 Nm
Speed n _{max}	
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	70 mm
	Oil/air

Tool interface

Interface	HSK-A 63
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Proximity switches
Taper cleaning	Air
Static tool pull-in force	18 kN
Seal	Air purge
Coolant	
through shaft	50 bar

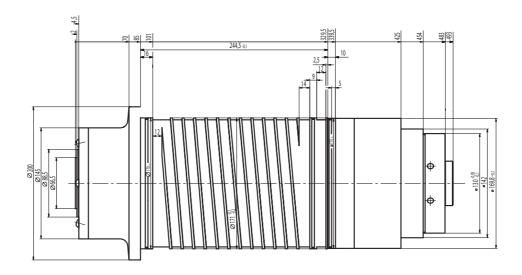
through shaft	50 bar
Diaidity	

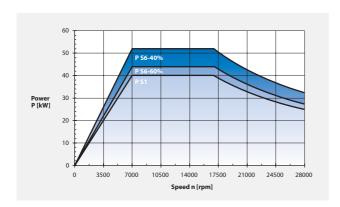
Rigidity Radial

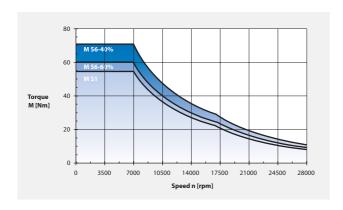
Radial	394 N/µm
Axial	297 N/µm



HCS 170 - 28000/40







Synchronous motor

Power P (S1)	40 kW at 7,000 rpm
Torque M (S1)	•
Speed n _{max}	28,000 rpm
Drive	closed-loop

Hybrid ball bearings

•	_	
Bore diameter		
of front bearing	S	.70 mm
Lubrication		.Oil/air

T

Tool interface	
Interface	HSK-A 63
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Proximity switches
Taper cleaning	Air
Seal	Air purge
Coolant	
through shaft	40 bar

Shaft movement

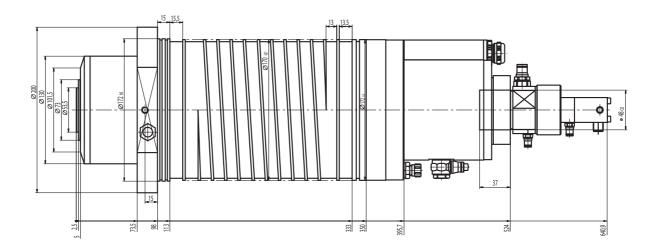
Compensating - AxialTemperature sensor

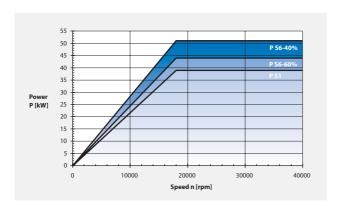
Rigidity

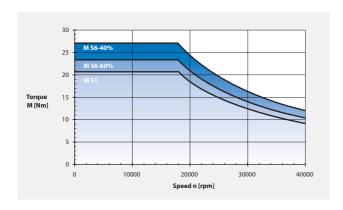
Radial	.410 N/μm
Axial	.190 N/um



HCS 170 - 40000/39







Asynchronous motor

Power P (S1)	39 kW at 18,000 rpm
Torque M (S1)	
Speed n _{max}	40,000 rpm
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	55 mm
Lubrication	

Tool interface

Interface	HSK-E 50
Monitoring	
"clamped", "unclamped"	Proximity switches
Taper cleaning	Air
Static tool pull-in force	10 kN

SealAir purge

Coolant

through shaft80 bar

Shaft movement

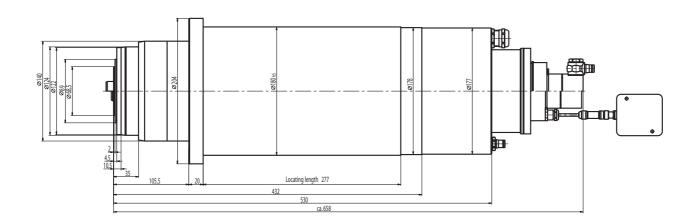
Compensating - Axial Temperature sensor Measuring - Axial Displacement sensor

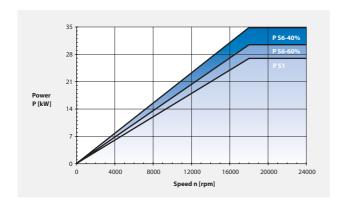
Rigidity

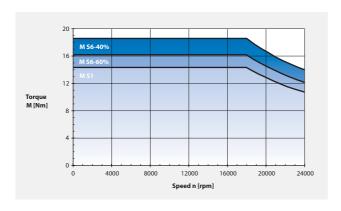
Radial	307	N/µm
Axial	102	N/um



HCS 180 - 24000/27







Asynchronous motor

Power P (S1)	27 kW at 18,000 rpm
Torque M (S1)	14.5 Nm
Speed n _{max}	
Drive	closed-loop

Hybrid ball bearings

Bore diameter of front bearings70 mm LubricationOil/air

Tool interface

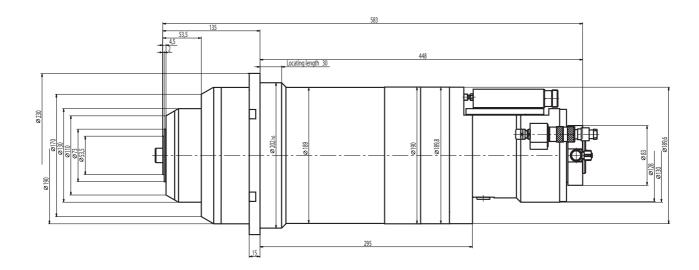
Interface	HSK-A 63
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Proximity switches
Taper cleaning	Air
Static tool pull-in force	18 kN
Seal	Air purge
Coolant	

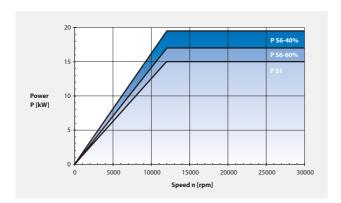
through shaft80 bar

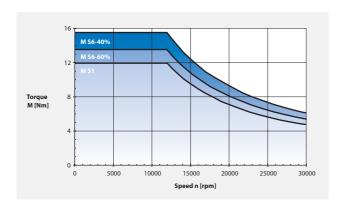
Radial440 N/µm Axial......290 N/μm



HCS 200 - 30000/15







Asynchronous motor

Power P (S1)	15 kW at 12,000 rpm
Torque M (S1)	12 Nm
Speed n _{max}	30,000 rpm
Drive	closed-loop

Hybrid ball bearings

Bore diameter		
of front bearings	55	mm
Lubrication		

Tool interface

Coolant	
SealAir purge	
Static tool pull-in force	11 kN
Taper cleaning	Air
"clamped without tool"	Proximity switches
"clamped", "unclamped",	
Monitoring	
Interface	HSK-A 50 / HSK-E 50

Coolant through shaft

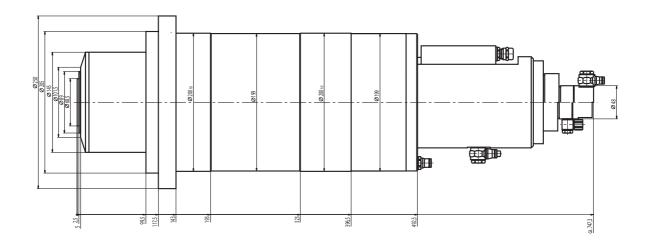
through shaft30 bar

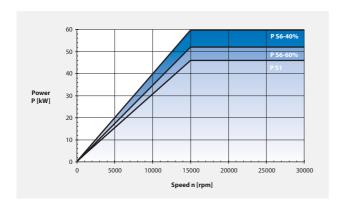
RigidityRadial.

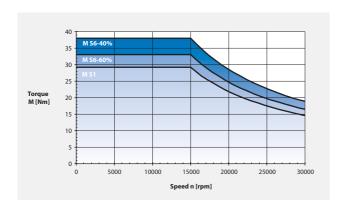
Radial	320 N/µm
Axial	110 N/µm



HCS 200 - 30000/46







Asynchronous motor

Power P (S1)	46 kW at 15,000 rpm
Torque M (S1)	29.3 Nm
Speed n _{max}	30,000 rpm
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	70 mm
Lubrication	Oil/air

Tool interface

Interface	HSK-E 63
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Proximity switches
Taper cleaning	Air
Static tool pull-in force	18 kN
Seal	Air purge
Coolant	

through shaft80 bar

Shaft movement

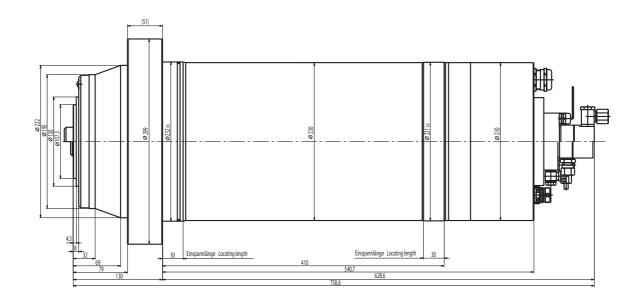
Measuring - Axial Displacement sensor

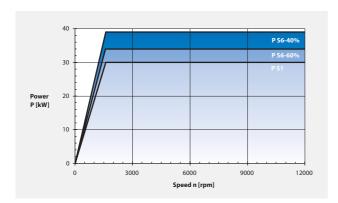
Rigidity

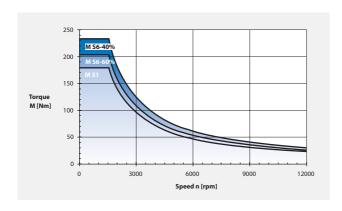
Radial422 N/µm Axial......128 N/μm



HCS 230 - 12000/30







Asynchronous motor

Power P (S1)	30 kW at 1,600 rpm
Torque M (S1)	
Speed n _{max}	
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	. 110 mm
Lubrication	.Oil/air

Tool interface

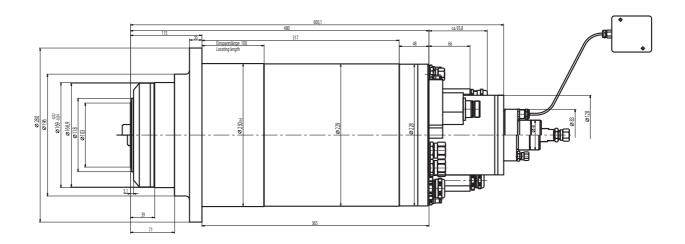
Interface	HSK-A 100
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	45 kN
Seal	Air purge
Coolant	
through shaft	50 bar
through spindle housing	3 bar

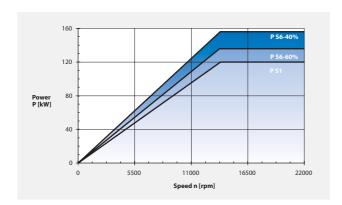
Rigidity

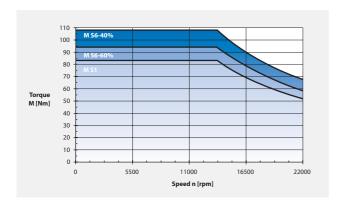
Radial	800	N/µm
Axial	320	N/um



HCS 230 - 22000/120







Power P (S1)	120 kW at 13,800 rpm
Torque M (S1)	83.5 Nm
Speed n _{max}	22,000 rpm
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	90 mm
Lubrication	Oil/air

Tool interface

Interface	HSK-A 80
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Proximity switches
Taper cleaning	Air
Static tool pull-in force	32 kN
Seal	Air purge
Coolant	
through shaft	50 bar

Shaft movement

Compensating - Axial	Temperature sensor
Measuring - Axial	Displacement senso
Measuring - Radial	2 Displacement

sensors

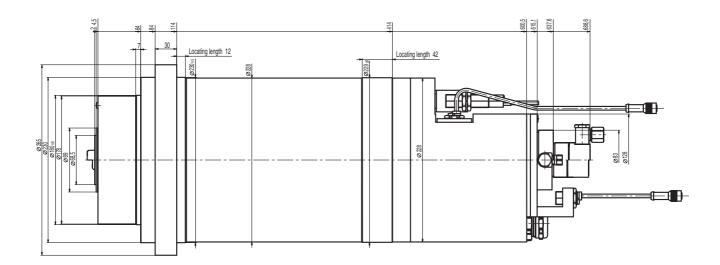
Vibration recognition Sensor

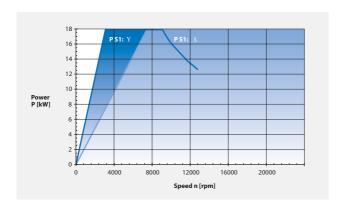
Rigidity

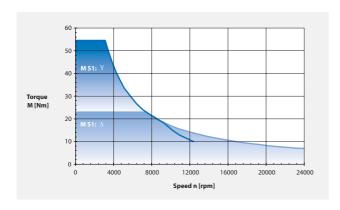
Radial	496	N/	μm
Axial	160	N/	μm



HCS 230 - 24000/18







Asylicili olious illotoi	
Star-Delta switching	
Power P (S1)	

Power P (S1)	. 18 kW at 3,150 rpm
Torque M (S1)	.57 Nm
Speed n _{max}	. 24,000 rpm
Drive	. closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	70 mm
Lubrication	Oil/air
Bearing preload	adjustable

Tool interface

Interface Monitoring	HSK-A 63
"clamped", "unclamped",	
"clamped without tool"	Proximity switches
	or Analog sensor
Taper cleaning	Air
Static tool pull-in force	18 kN
Seal	Air purge
Coolant	
through spindle housing	3 bar

Shaft movement

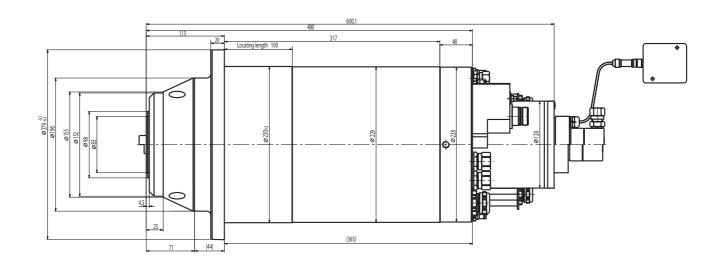
Compensating - AxialTemperature sensor

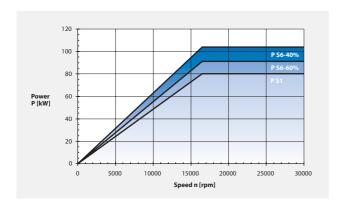
Rigidity

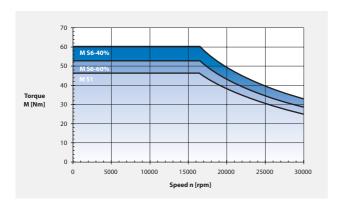
Radial	393 N/µm
Axial	130 N/um



HCS 230 - 30000/80







Async	hronous	motor
M3 VIIC	III OIIOUS	IIIOLUI

Power P (S1)	80 kW at 16,500 rpm
Torque M (S1)	•
Speed n _{max}	
Drive	closed-loon

Hybrid ball bearings

Bore diameter	
of front bearings	70 mm
Lubrication	

Interface.....HSK-A 63

Tool interface

Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	20 kN
Seal	Air purge

Shaft movement

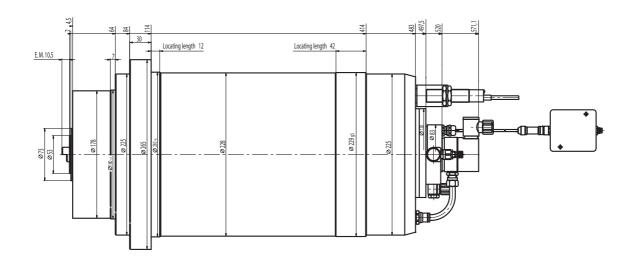
Compensating - Axial	Temperature sensor
Measuring - Axial	Displacement sensor
Measuring - Radial	2 Displacement
	sensors

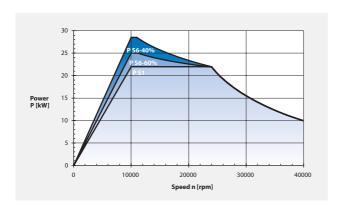
Vibration recognition Sensor **Rigidity**

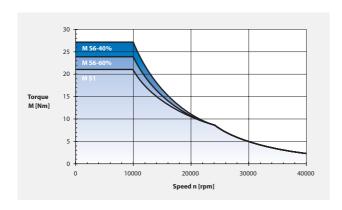
Radial	380	N/	μm
Axial	140	N/	μm



HCS 230 - 40000/22







Asynchronous motor

Power P (S1)	22 kW at 10,000 rpm
Torque M (S1)	21 Nm
Speed n _{max}	
Drive	

Hybrid ball bearings

•	•	
Bore diameter		
of front bearings	5	55 mm
Lubrication		Oil/air

Tool interface

Interface	HSK-E 50
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	10 kN
Seal	Air purge

Shaft movement

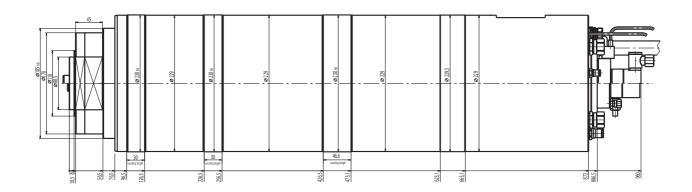
Compensating - AxialTemperature sensor

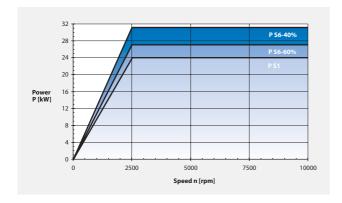
Rigidity

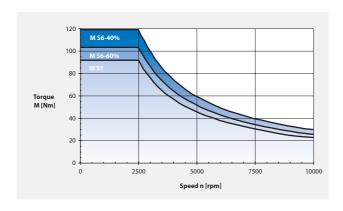
Radial260 N/µm Axial130 N/µm



HCS 230g - 10000/24







Asynchronous motor

Power P (S1)	24 kW at 2,500 rpm
Torque M (S1)	
Speed n _{max}	
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	90 mm
Lubrication	Grease

Tool interface

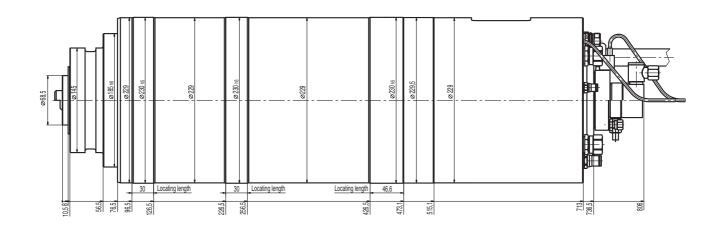
Interface	HSK-A 63
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	18 kN
Seal	Air purge
Coolant	
through shaft	50 bar

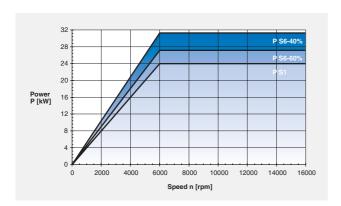
Rigidity

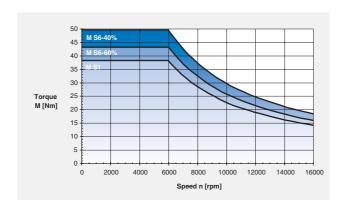
Radial	600 N/μm
Axial	430 N/um



HCS 230g - 16000/24







Asynchronous motor Power P (\$1)

Power P (S1)	24 kW at 6,000 rpm
Torque M (S1)	
Speed n _{max}	
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	.70 mm
Lubrication	.Grease

Tool interface

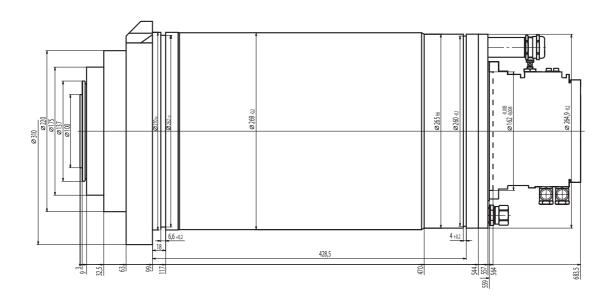
Interface	HSK-A 63
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	18 kN
Seal	Air purge
Coolant	
through shaft	50 bar

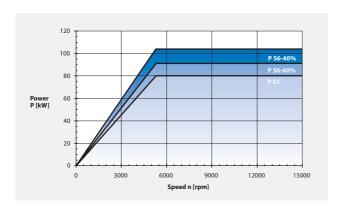
Rigidity

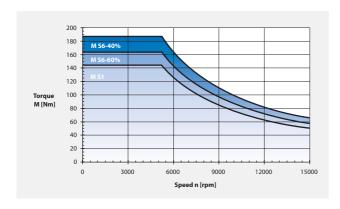
Radial	454 N/μm
Axial	317 N/um



HCS 270 - 15000/80







Asynchronous motor

Power P (S1)	80 kW at 5,340 rpm
Torque M (S1)	143.5 Nm
Speed n _{max}	
Drive	closed-loop

Hybrid ball bearings

•	•	
Bore diameter		
of front bearings	•••••	110 mm
Lubrication		

Tool interface

Interface	HSK-A 100
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Proximity switches
Taper cleaning	
Static tool pull-in force	45 kN
Seal	Air purge

Coolant

through shaft80 bar

Shaft movement

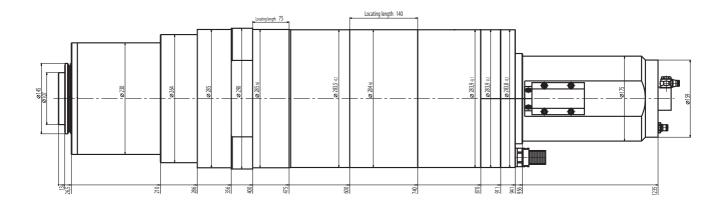
Compensating - AxialTemperature sensor

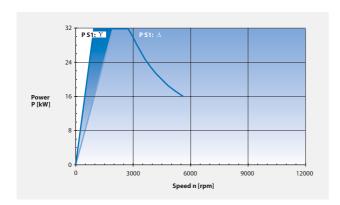
Rigidity

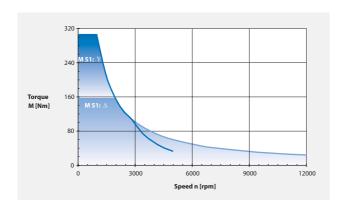
Radial728 N/μm Axial452 N/μm



HCS 285 - 12000/32







Asynchronous motor

Star-Delta switching	
Power P (S1)	32 kW at 1,000 rpm
Torque M (S1)	306 Nm
Speed n _{max}	
Drive	closed-loop

Hybrid ball bearings

Bore diameter	
of front bearings	110 mm
Lubrication	

Tool interface

Interface	HSK-A 100
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Proximity switches
Taper cleaning	Air
Static tool pull-in force	45 kN
Seal	Air purge

Coolant

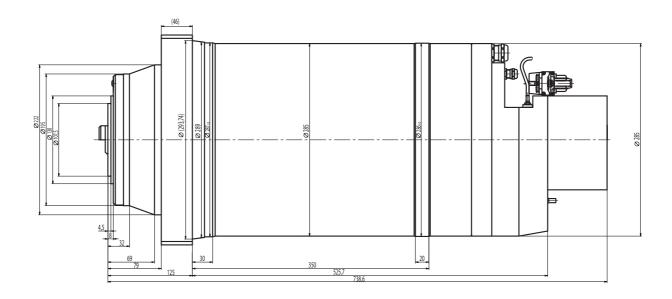
through shaft	80 ba
through spindle housing	4 bar

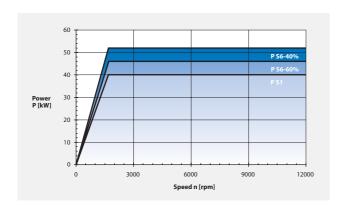
Rigidity

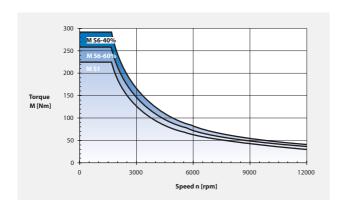
Radial	1,030 N/µm
Axial	600 N/um



HCS 285 - 12000/40







Async	hronous	motor
M3 VIIC	III OIIOUS	IIIOLUI

Power P (S1)	40 kW at 1,680 rpm
Torque M (S1)	227.5 Nm
Speed n _{max}	12,000 rpm
Drive	closed-loop

Hybrid ball bearings

,	
Bore diameter	
of front bearings	110 mm
	Oil/air

Tool interface

Interface	HSK-A 100
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	45 kN
Seal	Air purge

Coolant

through shaft	.80 bar
through spindle housing	3 bar

Shaft movement

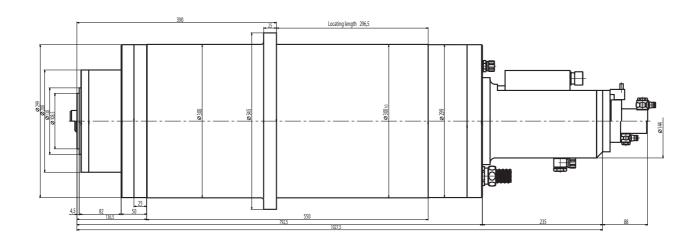
Compensating - AxialTemperature sensor

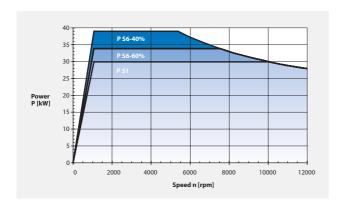
Rigidity

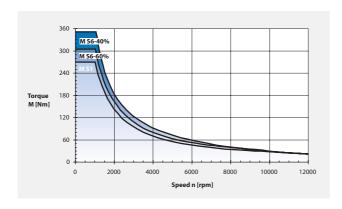
igiaity	
Radial	760 N/µm
Axial	350 N/µm



HCS 300 - 12000/30







Asynchronous motor

Power P (S1)	30 kW at 1,000 rpm
Torque M (S1)	270 Nm
Speed n _{max}	12,000 rpm
Drive	closed-loop

Hybrid ball bearings

bore diameter	
of front bearings	110 mm
Lubrication	Oil/air

Tool interface

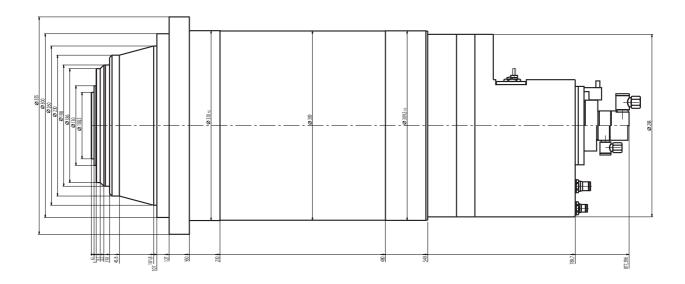
Interface	HSK-A 100
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	45 kN
Seal	Air purge
Coolant	

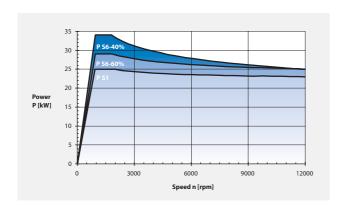
through shaft50 bar **Rigidity**

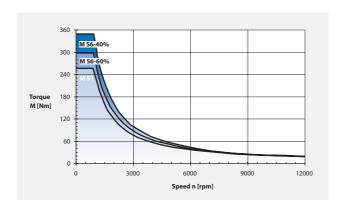
Radial	955 N/µm
Axial	607 N/µm



HCS 310 - 12000/25







Power P (S1)	25 kW at 930 rpm
Torque M (S1)	256,7 Nm
Speed n _{max}	12,000 rpm
Drive	closed-loop

Hybrid ball bearings

,	
Bore diameter	
of front bearings	110 mm
Lubrication	

Tool interface

Interfac	e	HSK-A 100
Monitor	ring	
"clampe	ed", "unclamped",	
"clampe	ed without tool"	Proximity switches
Taper cl	eaning	Air
Static to	ool pull-in force	45 kN
Seal		Air purge

Coolant

through shaft80 bar

Shaft movement

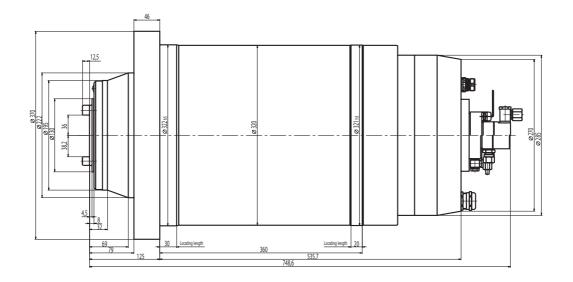
Compensating - AxialTemperature sensor

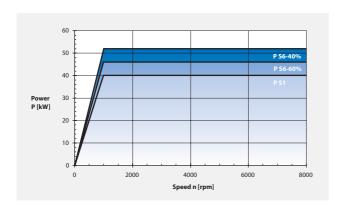
Rigidity

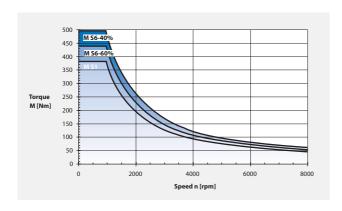
Radial 1,012 N/μm Axial607 N/μm



HCS 320 - 8000/40







Asynchronous motor

Power P (S1)	40 kW at 1,050 rpm
Torque M (S1)	380 Nm
Speed n _{max}	8,000 rpm
Drive	

Hybrid ball bearings

bore diameter	
of front bearings	110 mm
Lubrication	Oil/air

Tool interface

Interface	SK 50
Monitoring	
"clamped", "unclamped",	
"clamped without tool"	Analog sensor
Taper cleaning	Air
Static tool pull-in force	25 kN
Seal	Air purge
Coolant	
	001

C

through shaft	80 bar
through spindle housing	3 bar

Rigidity

Radial	760 N/μm
Axial	350 N/um